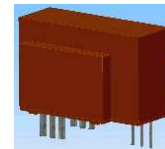


K-No.: 26392

### 25A Current Sensor

For the electronic measurement of currents:  
DC, AC, pulsed, mixed with a galvanic Isolation  
between the primary circuit (high power) and the  
secondary circuit (electronic circuit)



Date: 05.03.2018

Customer: Standard type

Customers Part no:

Page 1 of 5

#### Description

- Closed loop (compensation)  
Current Sensor with magnetic probe
- Printed circuit board mounting
- Casing and materials UL-listed

#### Characteristics

- excellent accuracy
- very low offset current
- very low temperature dependency and offset current drift
- very low hysteresis of offset current
- short response time
- wide frequency bandwidth
- compact design
- reduced offset ripple

#### Applications

Mainly used for stationary operation in industrial applications:

- AC variable speed drives and servo motor drives
- static converters for DC motor drives
- Battery supplied applications
- Switched Mode Power Supplies (SMPS)
- Power supplies for welding applications
- Uninterruptable Power Supplies (UPS)

#### Electrical data - Ratings

$I_{PN}$	Primary nominal RMS current	25	A
$R_M$	Measuring resistance	$V_C = \pm 12V$ $V_C = \pm 15V$	$10 \dots 200 \Omega$ $22 \dots 400 \Omega$
$I_{SN}$	Secondary nominal RMS current	25	mA
$K_N$	Transformation ratio	1...3:1000	

#### Accuracy – Dynamic performance data

		min.	typ.	max.	Unit
$I_{P,max}$	Max. measuring range				
	@ $V_C = \pm 12V$ , $R_M = 10 \Omega$ ( $t_{max} = 10sec$ )	$\pm 120$			A
	@ $V_C = \pm 15V$ , $R_M = 22 \Omega$ ( $t_{max} = 10sec$ )	$\pm 130$			A
X	Accuracy @ $I_{PN}$ , $\theta_A = 25^\circ C$		0.1	0.5	%
$\epsilon_L$	Linearity			0.1	%
$I_O$	Offset current @ $I_P = 0A$ , $\theta_A = 25^\circ C$		0.02	0.1	mA
$t_r$	Response time		500		$\mu s$
$t_{ra}$	Reaction time at $di/dt = 100 A/\mu s$		200		$\mu s$
$f_{BW}$	Frequency bandwidth	DC...200			kHz

#### General data

$\vartheta_A$	Ambient operation temperature	-40		85	$^\circ C$
$\vartheta_S$	Ambient storage temperature	-40		90	$^\circ C$
m	Mass		12		g
$V_C$	Supply voltage	$\pm 11.4$	$\pm 12/\pm 15$	$\pm 15.75$	V
$I_C$	Supply current at $I_P = 0A$ and RT		15		mA
* $S_{clear}$	Clearance (component without solder pad)	10.2			mm
* $S_{creep}$	Creepage (component without solder pad)	10.2			mm
* $U_{sys}$	System voltage			600	$V_{RMS}$
* $U_{AC}$	Working voltage			1000	$V_{RMS}$
* $U_{PD}$	Rated discharge voltage			1414	$V_S$
	Max. Potential difference acc. to UL 508			600	$V_{AC}$

\* Constructed, manufactured and tested in accordance with IEC 61800-5-1:2007 (primary to secondary)  
Reinforced insulation, Insulation material group 1, Pollution degree 2, Overvoltage category III

Date	Name	Issue	Amendment
05.03.2018	KRe	81	Sheet 4) other instruction changed ( PCBA is covered with conformal coating added). CN-18-044
13.08.2015	DJ	81	Marking with UL-sign, General data, routine-tests, Type-tests and Page 5 reworked. CN-15-419

Hrg.: R&D-PD NPI  
editor

Bearb.: DJ  
designer

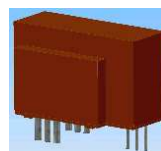
KB-PM: Sn.  
check

freig.: Pr.  
released

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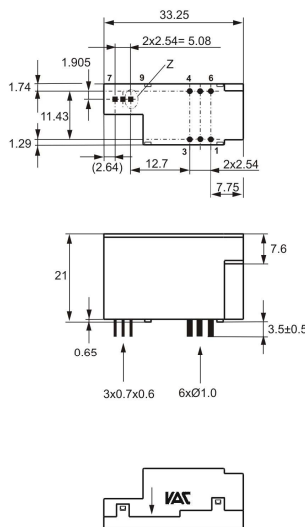
Page 2 of 5

#### Mechanical outline (mm):

General tolerances DIN ISO 2768-c

Connections:

Pin Nr. 1-6: Ø1,0mm  
Pin Nr. 7-9: 0,7 x 0,6mm



Tolerances of grid distance  
±0,2mm



Marking

Marking:

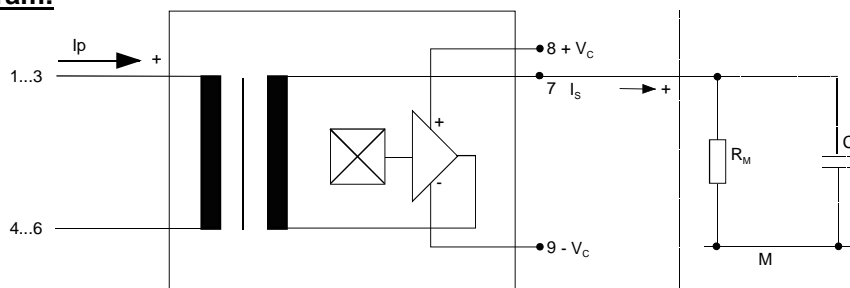
4648-X400  
F DC

Explanation:

DC = Date Code  
F = Factory

Current direction: A positive output current appears at point  $I_S$ , if primary current flows in direction of the arrow.

#### Schematic diagram:



#### Possibility of wiring for $V_C = \pm 15V$ (@ $\theta_A = 85^\circ C$ , $R_M = 22\Omega$ )

Primary-windings	Primary current RMS	Primary current peak	Output current RMS	Transformation-ratio	Primary-resistance	circuit
$N_P$	$I_P$ [A]	$\hat{I}_{P,max}$ [A]	$I_S(I_P)$ [mA]	$K_N$	$R_P$ [mΩ]	

1	25	130	25	1:1000	0,3	
2	10	65	20	2:1000	1,35	
3	8	43	24	3:1000	2,4	

Hrg.: R&D-PD NPI  
editor

Bearb.: DJ  
designer

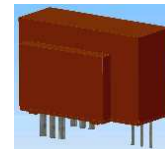
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Page 3 of 5

#### Electrical data (investigate by a type checking)

		min.	typ.	max.	Unit
$V_{C,tot}$	maximum supply voltage (without function) $\pm 15,75V$ to $\pm 18V$ : for 1s per hour			$\pm 18$	V
$R_S$	Secondary coil resistance @ $T_A = 85^\circ C$			88	$\Omega$
$R_P$	Primary coil resistance per turn @ $T_A = 25^\circ C$			1	m $\Omega$
$X_{TI}$	Temperature drift of X @ $T_A = -40^\circ C \dots 85^\circ C$			0.1	%
$I_{O,ges}$	Offset current (including $I_O, I_{Ot}, I_{OT}$ )			0.15	mA
$I_{Ot}$	Long term drift offset current von $I_O$		0.05		mA
$I_{OT}$	Offset current temperature drift $I_O$ @ $T_A = -40^\circ C \dots 85^\circ C$		0.05		mA
$I_{OH}$	Hysteresis current @ $I_P = 0A$ (caused by $I_P = 3 \times I_{PN}$ )		0.04	0.1	mA
$\Delta I_O / \Delta V_C$	Supply voltage rejection ratio			0.01	mA/V
$i_{OSS}$	Offsetripple* (with 1 MHz-Filter, first order)			0.4	mA
$i_{OSS}$	Offsetripple* (with 100 kHz-Filter, first order)		0.025	0.15	mA
$i_{OSS}$	Offsetripple* (with 20 kHz-Filter, first order)		0.001	0.04	mA
$C_k$	Maximum possible coupling capacity (primary - secondary)			6	pF
	Mechanical stress according to M3209/3 Settings: 10-2000Hz, 1min/oct, 2 hours			10	g

#### Routine-Tests: (Measurement after temperature balance of the samples at room temperature, SC = significant characteristic)

$K_N$ (SC)	(100%) M3011/6:	Transformation ratio		$3:1000 \pm 0,5 \%$	
$I_O$	(100%) M3226:	Offset current		< 0.1	mA
$U_P$	(100%) M3014:	Test voltage, 1s		2.5	kV <sub>RMS</sub>
$U_{PDE}$	(AQL 1/S4)	Partial discharge voltage (extinction)		1.5	kV <sub>RMS</sub>
$U_{PD} * 1.875$	M3024:	*acc. table 24		1.875	kV <sub>RMS</sub>

#### Type-Tests: (Precondition acc. to M3236)

$\hat{U}_W$		HV transient test acc. table 18,19 (1,2 $\mu$ s / 50 $\mu$ s-Waveform)		8	kV
$U_P$		Test voltage acc. to M3014, 5s		5	kV <sub>RMS</sub>
$U_{PDE}$		Partial discharge voltage (extinction)		1.5	kV <sub>RMS</sub>
$U_{PD} * 1.875$		*acc. table 24		1.875	kV <sub>RMS</sub>

\*IEC 61800-5-1:2007

Hrg.: R&D-PD NPI  
editor

Bearb.: DJ  
designer

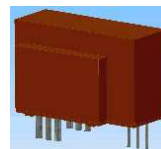
KB-PM: Sn.  
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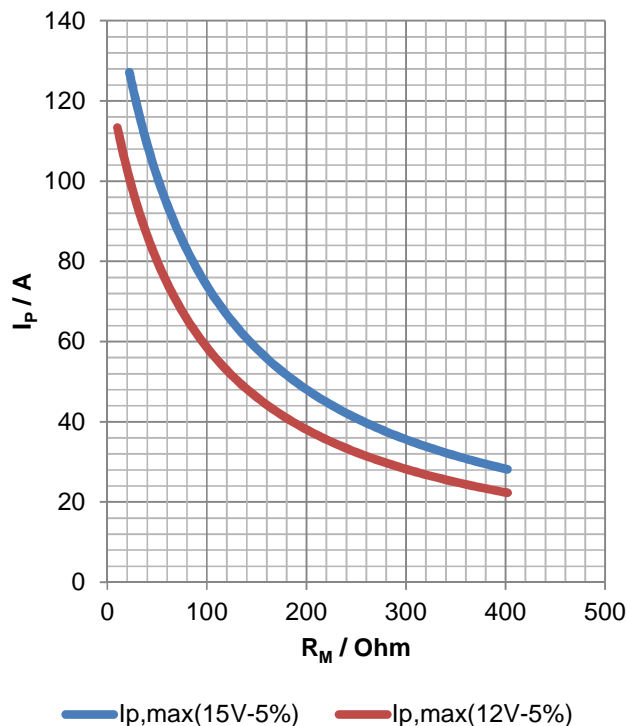
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Customer: Standard type

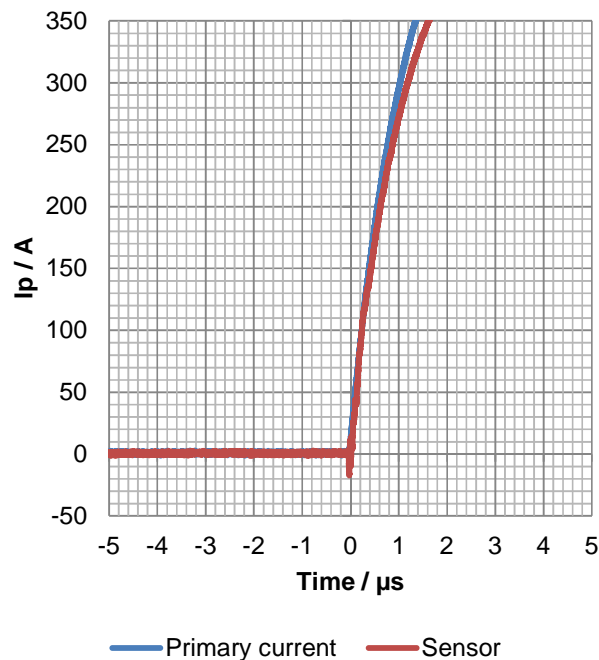
Customers Part no:

Page 4 of 5

**Limit curve of measurable current of N4648-X400**



**4648-X400, R<sub>m</sub> = 10Ω, I<sub>p</sub> = 500A**



Fast increasing currents (higher than the specified I<sub>p,max</sub>), e.g. in case of a short circuit, can be transmitted because the currents are transformed directly and be limited by diodes only.

### \*Possible way to reduce the Offset ripple by a Low-Pass-Filter

The offset ripple can be reduced by an external low pass. Simplest solution is a passive low pass filter of 1<sup>st</sup> order with cutoff frequency:

$$f_g = \frac{1}{2 * \pi * R_M * C_a}$$

In this case the response time is enlarged:

$$t'_r \leq t_r + 2,5R_M C_a$$

### Other instructions

- An exceptionally high rate of on/off – switching of the power supply voltage accelerates the aging process of the sensor
- Constructed, manufactured and tested in accordance with IEC 61800-5-1:2007.
- Temperature of the primary conductor should not exceed 100°C.
- Housing and bobbin material UL-listed: Flammability class 94V-0.
- PCBA is covered with conformal coating

Hrg.: R&D-PD NPI  
editor

Bearb.: DJ  
designer

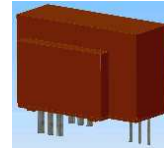
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Page 5 of 5

#### Explanation of several terms used in the tables:

$I_{OH}$ : Zero variation after overloading with a DC of tenfold the rated value. ( $R_M=R_{MN}$ )

$I_{oi}$ : Long term drift of  $I_o$  after 100 temperature cycles in the range  $-40^{\circ}\text{C}$  to  $85^{\circ}\text{C}$

$t_r$ : Response time, measured as a delay time at  $I_P = 0.9 * I_{Pmax}$  between a rectangular primary current and the output current.

$t_{ra}$ : Reaction time, measured as a delay time at  $I_P = 0.1 * I_{Pmax}$  between a rectangular primary current and the output current. (with  $di/dt = 100\text{A}/\mu\text{s}$ )

$X_{ges}(I_{PN})$ : The sum of all possible errors over the temperature range by measuring a current  $I_{PN}$ :

$$X_{ges} = 100 * \left| \frac{I_S * (I_{PN})}{K_N * I_{PN}} - 1 \right|$$

$X$ : Permissible measurement error in the final inspection at RT, defined by

$$X = 100 * \left| \frac{I_{SB}}{I_{SN}} - 1 \right|$$

where  $I_{SB}$  is the output DC value of an input DC current of the same magnitude as the (positive) rated current ( $I_o=0$ ).

$X_{Ti}$ : Temperature drift of the rated value orientated output term.  $I_{SN}$  in a specified temperature range, obtained by:

$$X_{Ti} = 100 * \left| \frac{I_{SB}(T_{A2}) - I_{SB}(T_{A1})}{I_{SN}} \right|$$

$\epsilon_L$ : Linearity fault defined by:  $\epsilon_L = 100 * \left| \frac{I_P}{I_{PN}} - \frac{I_{Sx}}{I_{SN}} \right|$

Where  $I_P$  is any input DC current and  $I_{Sx}$  the corresponding output term. ( $I_o = 0$ ).

